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# The relationship between fragility, configurational entropy and the potential energy landscape of glass-forming liquids

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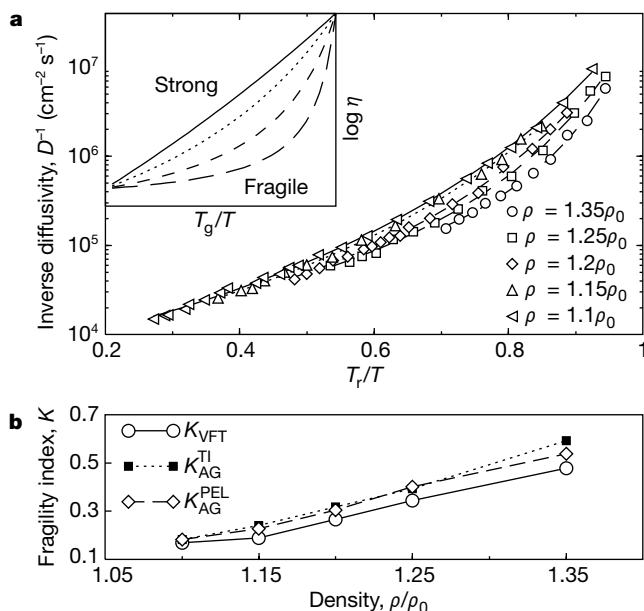
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Glass is a microscopically disordered, solid form of matter that results when a fluid is cooled or compressed in such a manner that it does not crystallize. Almost all types of materials are capable of glass formation, including polymers, metal alloys and molten salts. Given such diversity, general principles by which different glass-forming materials can be systematically classified are invaluable. One such principle is the classification of glass-formers according to their fragility<sup>1</sup>. Fragility measures the rapidity with which a liquid's properties (such as viscosity) change as the glassy state is approached. Although the relationship between the fragility, configurational entropy and features of the energy landscape (the complicated dependence of energy on configuration) of a glass-former have been analysed previously<sup>2</sup>, a detailed understanding of the origins of fragility is lacking. Here I use simulations to analyse the relationship between fragility and quantitative measures of the energy landscape for a model liquid whose fragility depends on its bulk density. The results reveal that fragility depends on changes in the vibrational properties of individual energy minima in addition to their total number and spread in energy. A thermodynamic expression for fragility is

derived, which is in quantitative agreement with kinetic fragilities obtained from the liquid's diffusivity.

Glass-forming liquids grow increasingly viscous upon cooling, till the viscosity becomes so large that they fail to flow on experimental timescales. While remaining microscopically disordered like a liquid, they manifest mechanical properties of a solid; that is, they transform to a glass. By convention, the glass transition temperature  $T_g$  is where the viscosity reaches a value of  $10^{12}$  Pa s. The approach to this large viscosity, however, differs from one liquid to another. When displayed in an Arrhenius plot of  $\log(\text{viscosity})$  versus inverse temperature  $1/T$ , some liquids (such as silica) show a steady, linear increase, while others display a much steeper dependence on  $1/T$  (refs 1, 3), as illustrated in Fig. 1a (inset). The former are 'strong' liquids, and the latter, 'fragile'. This range of behaviour is implicit in the Vogel–Fulcher–Tammann–Hesse (VFT) form, observed to describe the  $T$  dependence of viscosity (as well as diffusivity and relaxation times) in many glass-formers. The VFT relation may be written as:

$$\eta = \eta_0 \exp \left[ \frac{1}{K_{\text{VFT}}(T/T_0 - 1)} \right] \quad (1)$$



**Figure 1** Fragility plot of diffusivities, and kinetic and thermodynamic fragility indices. Results shown are obtained from molecular dynamics simulations of 204 A-type and 52 B-type particles interacting via the Lennard–Jones (LJ) potential. Argon units are used for A-type particles: LJ parameter  $\epsilon_{AA} = k_B \times 119.8 \text{ K}$ ,  $\sigma_{AA} = 0.3405 \times 10^{-9} \text{ m}$ ,  $m_A = 6.6337 \times 10^{-26} \text{ kg}$ ; and  $\epsilon_{AB}/\epsilon_{AA} = 1.5$ ,  $\epsilon_{BB}/\epsilon_{AA} = 0.5$ ,  $\sigma_{AB}/\sigma_{AA} = 0.8$ , and  $\sigma_{BB}/\sigma_{AA} = 0.88$ ,  $m_B/m_A = 1$ . Densities are reported in units of  $\rho_0 = 2.53 \times 10^{28} \text{ m}^{-3}$  or  $1.678 \text{ g cm}^{-3}$ . The liquid–gas critical point is located roughly at  $T_c = 130 \text{ K}$ ,  $\rho_c = 0.416\rho_0$ . **a**, Diffusivities  $D$  from molecular dynamics simulations (details of the simulations are as in ref. 10) are displayed in a ‘fragility plot’ for five densities. The reference temperature  $T_r$  is chosen such that  $D(T_r) = 2.44 \times 10^{-8} \text{ cm}^2 \text{ s}^{-1}$ , which is slightly below the lowest  $D$  values measured. The VFT extrapolation is used to locate  $T_r$ . Fitting values  $D_0$  (preexponent) are in the range of  $0.87$  to  $2.0 \times 10^{-4} \text{ cm}^2 \text{ s}^{-1}$ , close to the experimentally observed values. **b**, Fragility index  $K$  obtained (1) from VFT fits to diffusivities  $D$ ; and from the configurational entropy obtained (2) from thermodynamic integration (TI), and (3) from analysis of the potential energy landscape (PEL). Dimensionless thermodynamic fragility indices are obtained by dividing  $K_{\text{AG}}^{\text{TI}}$ ,  $K_{\text{AG}}^{\text{PEL}}$  by  $N\epsilon_{AA}$ . Comparison with data in ref. 11 shows that at the low-density end, the fragility of the model liquid compares with that of considerably fragile liquids such as toluene, orthoterphenyl and salol, while at the high-density end, the fragility is extremely high. Temperatures of vanishing diffusivity  $T_0$  from VFT fits are 18.76 K, 24.98 K, 35.97 K, 47.86 K and 75.75 K for  $\rho/\rho_0 = 1.1, 1.15, 1.2, 1.25$  and  $1.35$  respectively.

where  $T_0$  is the temperature of apparent divergence of viscosity, and  $K_{VFT}$  is a material-specific parameter quantifying the kinetic fragility; more fragile liquids have larger  $K_{VFT}$  values. This behaviour of viscosity correlates with the jump in heat capacity at the glass transition—the more fragile the liquid, the sharper and bigger the jump. Rationalization of this correlation comes from the Adam–Gibbs relationship<sup>4</sup> which predicts a dependence of viscosity on the configurational entropy  $S_c$  (described later) of the liquid:

$$\eta = \eta_0 \exp \left[ \frac{A}{TS_c} \right] \quad (2)$$

which results in the VFT relation if  $S_c$  has the form  $TS_c = K_{AG}(T/T_K - 1)$  (ref. 5), where  $T_K$  is the ideal glass transition or Kauzmann temperature<sup>4</sup> below which  $S_c = 0$ . The jump in heat capacity is proportional to  $K_{AG}$ , and is larger for more fragile glass-formers.

Fragility is analysed here for a binary mixture of particles interacting via the Lennard–Jones potential, widely studied as a model glass-former<sup>6–10</sup>. The  $T$  dependence of diffusivity  $D$  (to characterize dynamics) and configurational entropy are obtained for a range of bulk densities  $\rho$ . The diffusivities  $D(\rho, T)$ , are shown in Fig. 1a in a ‘fragility plot’:  $-\log[D(\rho, T)]$  versus  $T_i/T$ , where  $T_i$  is a reference temperature (akin to  $T_g$  in the usual fragility plot) at which  $D$  at each density reaches a fixed, small value. By comparison with the inset, the liquid is seen to become more fragile as its density increases. Figure 1b shows the kinetic fragility index,  $K_{VFT}$ , obtained from VFT (equation (1)) fits to diffusivity data at each density. The density dependence of  $K_{VFT}$  quantifies the increase of fragility with density, apparent from data in Fig. 1a.

A thermodynamic explanation of fragility, as discussed above (also refs. 11, 12), lies in explaining the rapidity of change with  $T$  of the configurational entropy,  $S_c$ . In the inherent structure (IS) formalism<sup>13,14</sup> used here, the configuration space of a liquid is divided into basins of local potential energy minima (‘inherent structures’).  $S_c$  at a given  $T$  derives from the multiplicity of local potential energy minima sampled by the liquid at that  $T$ , and equals the difference of the total entropy and the vibrational entropy of typical basins sampled,  $S_{vib}$ :

$$S_c(\rho, T) = S_{total}(\rho, T) - S_{vib}(\rho, T) \quad (3)$$

For all the results presented here, the basin entropy  $S_{vib}$  is calculated by approximating each basin as a harmonic well (valid at sufficiently low  $T$ )<sup>8–10,15</sup>. In this approximation, the entropy of a given basin, arising from vibrational motion within the basin is given by:

$$S_{vib} = k_B \sum_{i=1}^{3N} 1 - \log \left( \frac{h\nu_i}{k_B T} \right) \quad (4)$$

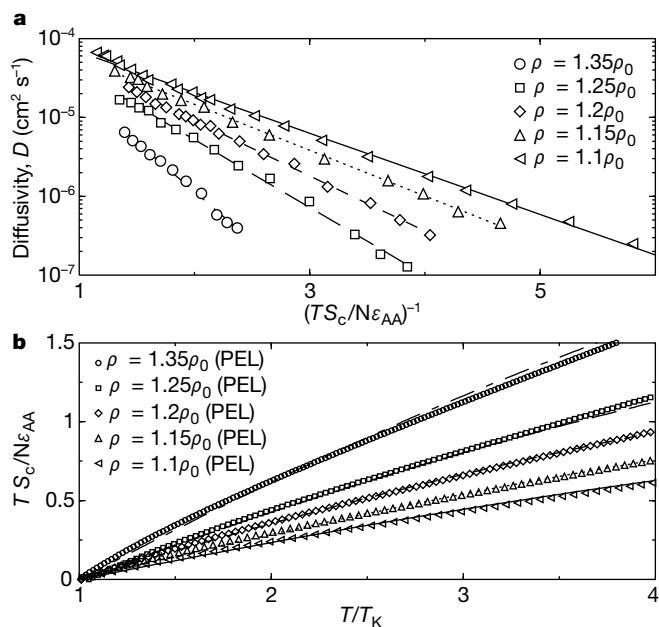
where  $\nu_i$  are the vibrational frequencies of the given basin,  $k_B$  is Boltzmann’s constant and  $h$  is Planck’s constant. The basin free energy is  $F_{vib} = U_{vib} - TS_{vib}$ , where  $U_{vib} = 3Nk_B T$  is the internal energy. Apart from the explicit temperature dependence of  $S_{vib}$  above, an implicit dependence also exists because vibrational frequencies change from one basin to another, and different basins are sampled at different temperatures. From the expression above, it is clear that the entropy difference between any two basins arises solely from the difference in their vibrational frequencies, and is independent of temperature.

The configurational entropy is evaluated here using two methods, referred to as the thermodynamic integration (TI) method, and the potential energy landscape (PEL) method, respectively. In both cases, inherent structures are obtained by performing local potential energy minimization for a subset of configurations sampled by a liquid at each  $\rho$  and  $T$ . Vibrational frequencies are calculated for each inherent structure, and the basin entropy  $S_{vib}$  is obtained from equation (4). In the TI method (described in detail elsewhere<sup>8–10</sup>; see

also caption of Fig. 2), the total entropy  $S_{total}$  is obtained using pressure and internal energy values from simulations. Equation (3) is used to obtain  $S_c$ . In contrast, the PEL method is based on constructing the distribution of inherent structures in order to calculate  $S_{total}$  and  $S_c$ , as described later.

Figure 2a shows the Adam–Gibbs plot, where  $\log D$  is plotted against  $(TS_c)^{-1}$ . The Adam–Gibbs relation (equation (2)) applies well at each density, as was also observed previously for the hard sphere liquid<sup>16</sup> and water<sup>17</sup>. Figure 2b shows (as lines) the  $T$ -dependence of  $TS_c$  (from TI). All curves are nearly linear, but with slight increases of slope at lower  $T$ . The slopes of  $TS_c$  (in the  $T$  range where diffusivities are measured),  $K_{AG}^{TI}$ , are used as the quantitative index of thermodynamic fragility, and are plotted in Fig. 1b.  $K_{AG}^{TI}$  are nearly the same as the kinetic fragility index  $K_{VFT}$ , thereby validating the idea that the rate of increase of  $TS_c$  does indeed determine the fragility.

However, this analysis provides no insight into how the fragility relates to features of the energy landscape. To this end, I now examine the distribution of energy minima, and properties of individual basins at fixed density  $\rho$ . The probability distribution  $P(\Phi, T)$  that an inherent structure of energy  $\Phi$  is sampled at temperature  $T$  depends on (1) the energy  $\Phi$ ; (2) the structure of



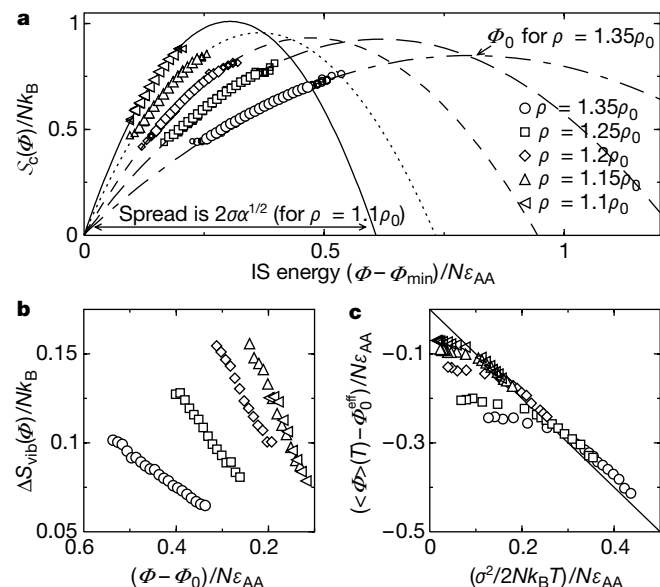
**Figure 2** Adam–Gibbs plot of configurational entropy versus temperature. **a**, The Adam–Gibbs plot displaying  $\log(D)$  versus  $(TS_c)^{-1}$ .  $TS_c$  is expressed in units of  $\epsilon_{AA}$ . The Adam–Gibbs expectation of a linear dependence is well satisfied at each density. **b**, Configurational entropy obtained from thermodynamic integration (TI) (lines, not labelled), and from analysis of the potential energy landscape (points, labelled PEL), plotted against temperature  $T$  scaled to the Kauzmann temperature  $T_K$  obtained from thermodynamic integration. In the TI method, the total entropy  $S_{total}$  of the liquid is obtained from its total free energy  $F_{total}$ , from  $F_{total} = U_{total} - TS_{total}$ , where  $U_{total}$  is the internal energy. Thermodynamic identity  $P = \rho^2((\partial F_{total}/N)/\partial \rho)_T$ , where  $P$  is the pressure, is used to integrate  $P$  from simulations to obtain  $F_{total}$  with respect to the known ideal-gas free energy. The identity  $U_{total} = ((\partial F_{total}/T)/(\partial 1/T))_\rho$  is used to integrate, at fixed density,  $U_{total}$  from simulations to obtain  $F_{total}$  at any desired  $T$ . Extrapolations to low  $T$  beyond the range of simulations use the form for the potential energies  $E$ ,  $E = E_0 + E_1 T^{\epsilon_2}$ , where  $E_2 \approx 3/5$  (see refs 8–10). Basin entropies  $S_{vib}$  are obtained by averaging over typical inherent structures at each  $T$ , whose vibrational frequencies are obtained numerically by diagonalizing the Hessian (matrix of second derivatives of the potential energy). The plot covers at each density the range of  $T$  where simulations have been performed. Scaling temperatures  $T_K^I$ , the Kauzmann or ideal glass transition temperature where  $S_c = 0$ , are: 20.44 K, 26.83 K, 34.35 K, 42.49 K and 62.47 K, for  $\rho/\rho_0 = 1.1, 1.15, 1.2, 1.25$  and  $1.35$  respectively.  $T_K^{PEL}$  obtained from the PEL method are, in the same order: 20.24 K, 26.1 K, 34.7 K, 44.64 K and 62.35 K.

the basin, contained in the basin free energy  $F_{\text{vib}}(\Phi, T)$  and (3) the number density of inherent structures with energy  $\Phi$ ,  $\Omega(\Phi)$  (refs 8, 13–15, 18):

$$P(\Phi, T) = \Omega(\Phi) \exp[-\beta(\Phi + F_{\text{vib}}(\Phi, T))]/Q_N(\rho, T) \quad (5)$$

where  $Q_N$ , the partition function, normalizes  $P$  and is given by  $Q_N = \int d\Phi P(\Phi, T)$  over all possible  $\Phi$ . The configurational entropy density is defined by  $S_c(\Phi) \equiv k_B \ln \Omega(\Phi)$  and is related to the  $T$ -dependent configurational entropy by  $S_c(T) = \int d\Phi S_c(\Phi) P(\Phi, T)$ . The quantities  $P(\Phi, T)$ ,  $F_{\text{vib}}$  and  $Q_N$  are obtained from simulations<sup>8,10,15,18</sup>, and are used to invert the relation in equation (5) to obtain the configurational entropy density  $S_c(\Phi)$ . The same  $S_c(\Phi)$  estimates must result (through not for the same range of  $\Phi$ ) for different  $T$ , when the harmonic assumption is valid, which is confirmed by the data shown in Fig. 3a. With increasing density, the maximum  $S_c(\Phi)$  value reached decreases, and the distribution becomes broader. It has been argued<sup>19,30</sup> that the distribution  $\Omega(\Phi)$  should be gaussian (equivalently,  $S_c(\Phi)$  an inverted parabola). Data in Fig. 3a are fully consistent with this expectation, and are fitted to the form:

$$\frac{S_c(\Phi)}{Nk_B} = \alpha - \frac{(\Phi - \Phi_0)^2}{\sigma^2} \quad (6)$$



**Figure 3** Distribution of energy minima, basin entropy and temperature dependence of inherent structure energies. **a**, The configurational entropy  $S_c(\Phi)$  plotted against inherent structure energy  $\Phi$  minus the Kauzmann energy  $\Phi_{\text{min}}$  below which  $S_c(\Phi) = 0$ .  $\Phi_{\text{min}}$  is the lower root of  $S_c(\Phi)/Nk_B = \alpha - (\Phi - \Phi_0)^2/\sigma^2 = 0$ . For each density, data from nine temperatures (on average) are shown (smaller symbols) which collapse onto each other, validating the harmonic approximation for calculating basin entropies (see text). Also shown are the averages of these curves (larger symbols), for whose calculation a threshold of 20 samples (out of a total of 1,000) is imposed in each bin. **b**, The  $T$ -independent component of the basin entropy  $\Delta S_{\text{vib}}(\Phi)$  versus  $\Phi - \Phi_0$ , where  $\Phi_0$  is the value at which  $S_c(\Phi)$  is maximum.  $\Delta S_{\text{vib}}(\Phi)$  curves are approximately linear. The  $T$  independence of  $\Delta S_{\text{vib}}(\Phi)$  is an artefact of the classical mechanical treatment used here, but a quantum mechanical calculation of the basin entropy does not alter the picture fundamentally (unpublished results). **c**, Scaled plot of the average IS energies sampled in simulations, which are expected to collapse on the straight line shown at low temperatures (right side of the graph), if the assumption of a gaussian configurational entropy density  $S_c(\Phi)$  is valid (see text). The observed data collapse validates the gaussian form used for  $S_c(\Phi)$ . Deviations at high temperatures are due to the breakdown of harmonicity of the basins. Fitting parameters  $\alpha$ ,  $\Phi_0/N\epsilon_{AA}$ ,  $\sigma/N\epsilon_{AA}$  and  $\delta S_{\text{vib}}/k_B$  are: for  $\rho = 1.1\rho_0$ , 1.010, -6.586, 0.303, -0.721; for  $\rho = 1.15\rho_0$ , 0.957, -6.684, 0.374, -0.652; for  $\rho = 1.2\rho_0$ , 0.933, -6.683, 0.489, -0.500; for  $\rho = 1.25\rho_0$ , 0.927, -6.564, -0.314; and for  $\rho = 1.35\rho_0$ , 0.849, -6.088, 0.873, -0.188.

where  $\alpha$  is the height of the parabola and determines the total number of configurational states, that is, energy minima (the total number is proportional to  $\exp(\alpha N)$ ),  $\Phi_0$  and  $\sigma^2$  respectively define the mean and the variance of the distribution. The fits are displayed in Fig. 3a and the fit parameters listed in the legend. Speedy<sup>2</sup> has considered a model of the thermodynamics of a glass-former with a gaussian distribution of configurational states, and the basin specific heat that does not depend on the internal parameter (here, the IS energy). He predicts that the fragility of a liquid should be proportional to the logarithm of the number of states, that is to  $\alpha$ . From Fig. 3a it is clear that  $\alpha$  values, and hence the number of states, decrease with increasing density  $\rho$ . But the fragilities (Fig. 1b) show the opposite trend. However, fragility has an additional dependence (implicit in ref. 2) on the variance of the distribution,  $\sigma$  (see equation (6)).

Further, the variation of vibrational frequencies, and hence the basin entropy, from basin to basin, also contributes to the fragility of the liquid. Figure 3b displays the  $T$ -independent (see above) basin entropy difference at a given energy  $\Phi$  with respect to the value at  $\Phi_0$ ,  $\Delta S_{\text{vib}}(\Phi) \equiv S_{\text{vib}}(\Phi, T) - S_{\text{vib}}(\Phi_0, T)$ . At all densities,  $\Delta S_{\text{vib}}(\Phi)$  displays a clear  $\Phi$  dependence, which is inconsistent with assumptions in ref. 2. Although such basin dependence of vibrational frequencies and hence the basin entropy have been discussed<sup>20–29</sup>, with reference to both experimental data and model calculations, its effects on a liquid's fragility have not clearly been established. Figure 3b shows that basins at higher energy (occupied at higher temperature) have lower basin entropies or higher frequencies (see equation (3)). This trend, contrary to what one expects for systems studied experimentally, arises because the constant-density model system here cannot expand when  $T$  is raised.

The dependence of  $\Delta S_{\text{vib}}(\Phi)$  on  $\Phi$  is to a great extent linear. Hence, for each density,  $\Delta S_{\text{vib}}$  is fitted to the form  $\Delta S_{\text{vib}}(\Phi) = \delta S(\Phi - \Phi_0)$  with the fitting parameters listed in the legend of Fig. 3. The basin free energy, which can be written as  $F_{\text{vib}}(\Phi, T) = F_{\text{vib}}(\Phi_0, T) - T\delta S(\Phi - \Phi_0)$ , is also linear in  $\Phi$ . With a gaussian form for  $\Omega$ , the partition function  $Q_N = \int d\Phi P(\Phi, T)$  ( $P$  as in equation (5)) is easily evaluated, and results in the following predictions for the  $T$  dependence of the average IS energy, and the configurational entropy:

$$\langle \Phi \rangle(T) = \Phi_0^{\text{eff}} - \frac{\sigma^2}{2Nk_B T} \quad (7)$$

where  $\Phi_0^{\text{eff}} = \Phi_0 + \sigma^2 \delta S / 2Nk_B$ , and

$$T_S(T) = K_{\text{AG}}^{\text{PEL}}(T)(T/T_K - 1);$$

$$K_{\text{AG}}^{\text{PEL}}(T) = \left( \frac{\sigma\sqrt{\alpha}}{2} + \frac{\sigma^2 \delta S}{4Nk_B} \right) \left( 1 + \frac{T_K}{T} \right) - \frac{\sigma^2 \delta S}{2Nk_B} \quad (8)$$

where  $T_K = \sigma(2Nk_B\sqrt{\alpha} + \sigma\delta S)^{-1}$  is the ideal glass transition temperature where  $S_c(T_K) = 0$ .

The form above for  $S_c$  results in the VFT relation, if  $K_{\text{AG}}^{\text{PEL}}(T)$  is constant. This is not quite the case, but the  $1/T$  term becomes rapidly irrelevant for  $T > T_K$  and  $K_{\text{AG}}^{\text{PEL}}(T)$  approaches a constant. Further,  $T_S$  values plotted (as points) in Fig. 2b are in very good agreement with the ones from thermodynamic integration, including deviations from linearity for small  $T/T_K$ . A check of the overall consistency of the model described here is made in Fig. 3c, which shows a scaled plot of  $\langle \Phi \rangle(T) - \Phi_0^{\text{eff}}$  versus  $\sigma^2/2Nk_B T$ . From equation (7), one expects  $\langle \Phi \rangle(T)$  data for all densities to collapse onto a straight line of (negative) unit slope, with expected deviations at high  $T$  due to basin anharmonicity<sup>15</sup>. Data in Fig. 3c clearly meet this expectation, although with noticeable deviations for  $\rho = 1.35\rho_0$ , as also in Fig. 2b.

The expression for  $K_{\text{AG}}^{\text{PEL}}$  in equation (8), the thermodynamic fragility index obtained from energy landscape parameters, shows

that fragility depends not only on the multiplicity of states ( $\alpha$ ) but also on their spread ( $\sigma$ ), and how much the basin entropy changes from the lowest to the highest energy basins sampled by the liquid. The extent of this change is quantified by parameters  $\sigma$  and  $\delta S$  (listed in the caption of Fig. 3). Figure 1b shows the average slopes of  $TS_c$  (from equation (8) above, in the  $T$  range where diffusivities are measured),  $K_{AG}^{PEL}$ , which are nearly the same as  $K_{AG}^{IT}$ , and in very good agreement with the kinetic fragility index  $K_{VFT}$ . This agreement establishes the quantitative relationship between fragility and the energy landscape of the liquid, as  $K_{AG}^{PEL}$  is obtained solely in terms of a quantitative description of the liquid's energy landscape. □

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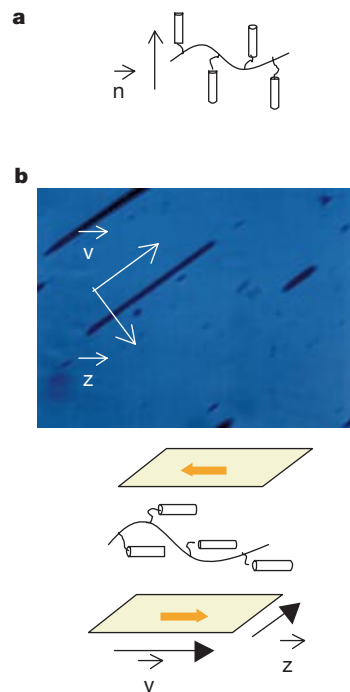
**Observation of shear-induced nematic–isotropic transition in side-chain liquid crystal polymers**

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Flow-induced phase transitions are a fundamental (but poorly understood) property of non-equilibrium systems, and are also of practical importance for tuning the processing conditions for plastics, petroleum products, and other related materials<sup>21</sup>. Recognition that polymers may exhibit liquid crystal properties has led to the discovery of the first tailored side-chain liquid crystal polymers (SCLCPs), which are formed by inserting a spacer between the main polymer chain and the lateral mesogen liquid–crystalline graftings<sup>22</sup>. Subsequent research has sought to understand the nature of the coupling between the main polymer chain and the mesogens, with a view to obtaining better control of the properties of these tailored structures<sup>22</sup>. We show here that the parallel or perpendicular orientation of the mesogens with respect to the main chain can be reversed by the application of an external field produced by a shear flow, demonstrating the existence of an isotropic nematic phase transition in SCLCPs. Such a transition, which was theoretically predicted<sup>1,2</sup> for low-molecular-weight liquid crystals but never observed, is shown to be a general property of SCLCPs too. We expect that these SCLCPs will prove to be good candidate systems for the experimental study of these non-equilibrium phenomena.

Side-chain liquid crystal polymers are made of mesogens (liquid crystal molecules) laterally attached to a conventional main-chain polymer (Fig. 1). The question of the orientation of the main-chain



**Figure 1** Behaviour of the side-chain liquid crystal polymer described in the text. **a**, Oblate main-chain conformation in the nematic phase, at equilibrium; **b**, strong birefringence due to the emergence of the shear-induced nematic phase (crossed-polarizer micrograph at  $\dot{\gamma} = 10 \text{ s}^{-1}$  and  $T - T_{NI} = 1.5^\circ\text{C}$ ), and corresponding shear-induced main-chain conformation.  $n$  is the phase direction,  $v$  the velocity and  $z$  the neutral axis.